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Estimating Multiphase Hydraulic Properties at a Crude-Oil Spill Site

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THREE-PHASE CAPILLARY PRESSURE CURVES:

Oil-water and air-oil capillary pressure curves were scaled from the estimated air-water curve using the methods of Lenhard and Parker (1988), which were based on the concepts of Leverett and Lewis (1941). In this model, the sediment remains water wet, and the oil spreads on water, completely covering the air-water interface. For example, the oil-water capillary pressure, P_{ow} , was assumed to be a function of the water saturation, and calculated from the air-water curve by incorporating a scaling factor into the Van Genuchten equation

$$S_w = [1 + (\beta_{ow}\alpha P_{ow})^n]^{-m},$$

where β_{ow} is the ratio of the air-water surface tension to the oil-water surface tension.

HYSTERESIS AND FLUID ENTRAPMENT

The hysteresis model we used was based on the work of Luckner, Van Genuchten, and Nielson (1989) and Kool and Parker (1987). For example, the main water wetting curve saturation was calculated from a modified Van Genuchten function:

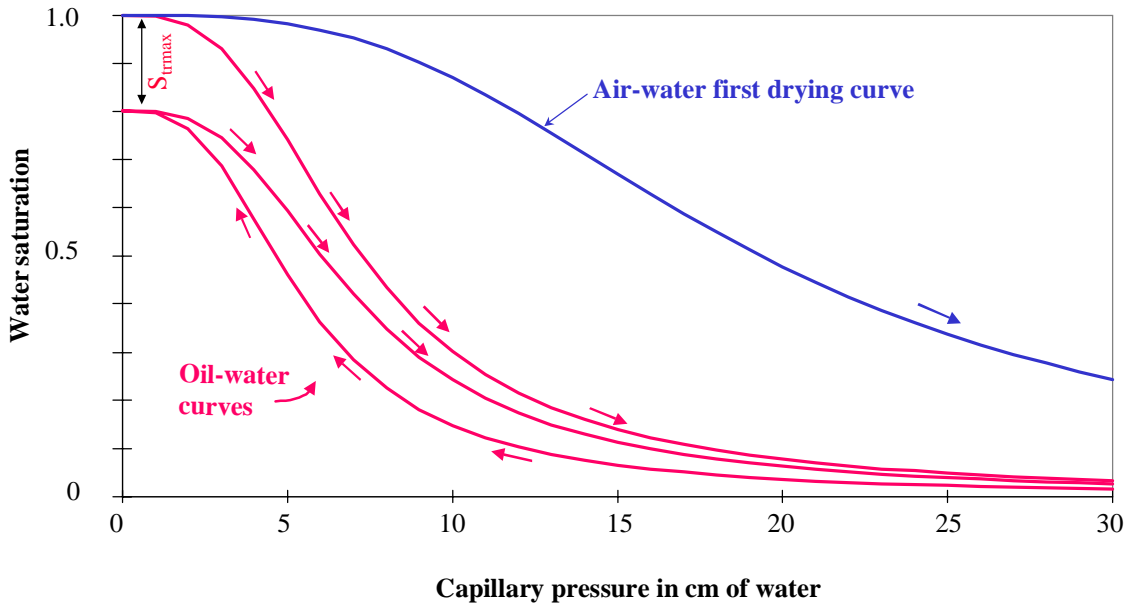
$$S_w = [1 - S_{tr}] [1 + (\beta_{ow}\alpha_w P_{ow})^n]^{-m},$$

where $\alpha_w = 1.3 \alpha$, and S_{tr} is the entrapped oil saturation. Oil entrapment was estimated using the model of Land (1968):

$$S_{tr} = S_{rev} / [1 - S_{rev} (1 - 1/S_{trmax})],$$

where S_{rev} is the oil saturation at which reversal from drying to wetting occurred, and S_{trmax} is the maximum oil entrapment. Air entrapment was assumed to be zero. It was assumed that in the time scales of interest, entrapped air dissolved in the water or in the oil. An example hysteretic curve is shown below.

Capillary pressure curve scaling



ESTIMATING RELATIVE PERMEABILITIES

At each grid point in the model aquifer, the water relative permeability, k_{rw} , was estimated using Mualem's (1976) expression:

$$k_{rw} = (S_w)^{1/2} \{1 - [1 - (S_w)^{1/m}]^m\}^2$$

where $m = 1 - 1/n$ comes from the capillary pressure curve fit. The oil relative permeability, k_{ro} , was calculated using the modified formula suggested by Parker et al. (1987):

$$k_{ro} = (S_t - S_w)^{1/2} \{[1 - (S_w)^{1/m}]^m - [1 - (S_t)^{1/m}]^m\}^2,$$

where S_t is the total liquid saturation.